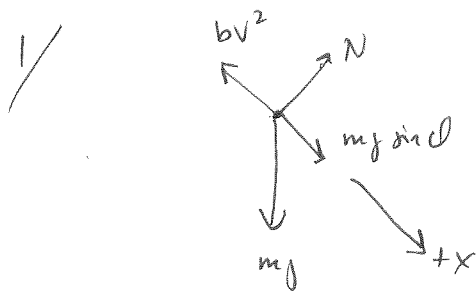


# Exam 1: Solution



$$F_x = m\ddot{x}$$

$$mg \sin \theta - bv^2 = m\dot{v}$$

- terminal velocity is when resistive force becomes as large as the driving force (here, gravity), so the object no longer accelerates  $\dot{v} = 0$  at  $v = v_{\text{terminal}}$

$$mg \sin \theta - bv_+^2 = 0$$

$$v_+ = \sqrt{\frac{mg \sin \theta}{b}}$$

2/

$$F_x = m\ddot{x}$$

$$-bv^{3/2} = m\dot{v}$$

$$\text{here, } \dot{v} = \frac{dv}{dt} = \frac{dv}{dx} \frac{dx}{dt} = \frac{dv}{dx} v$$

$$-bv^{3/2} = m \frac{dv}{dx} v$$

$$\int_0^{x_f} dx = \int_{v_0}^{v_f} -\frac{m}{b} \frac{dv}{\sqrt{v}}$$

$$x_f = \left(-\frac{m}{b}\right) (2) v^{1/2} \Big|_{v_0}^{v_f}$$

$$x_f = -\frac{2m}{b} (\sqrt{v_f} - \sqrt{v_0})$$

$$\text{if } v_f = 0$$

$$x_f = \frac{2m}{b} \sqrt{v_0}$$

3/ Consider a 3 particle system of internal forces  $\vec{F}_{12}, \vec{F}_{23}, \vec{F}_{21}, \vec{F}_{32}, \vec{F}_{31}, \vec{F}_{32}$  and external forces  $\vec{F}_{1ext}, \vec{F}_{2ext}, \vec{F}_{3ext}$

• the net force on the system is

$$\vec{F}_{net} = \vec{F}_{12} + \vec{F}_{13} + \vec{F}_{21} + \vec{F}_{23} + \vec{F}_{31} + \vec{F}_{32} + \vec{F}_{1ext} + \vec{F}_{2ext} + \vec{F}_{3ext} = \frac{d\vec{p}_T}{dt}$$

where  $\vec{F}_{net} = \frac{d\vec{p}_T}{dt}$  by Newton's 2nd law

• By Newton's third law,  $\vec{F}_{12} = -\vec{F}_{21}, \vec{F}_{23} = -\vec{F}_{32} + \vec{F}_{31} = -\vec{F}_{13}$ . These terms cancel.

$$\vec{F}_{net} = \vec{F}_{1ext} + \vec{F}_{2ext} + \vec{F}_{3ext} = \frac{d\vec{p}_T}{dt}$$

• In the case of no <sup>net</sup> external force,  $\frac{d\vec{p}_T}{dt} = 0$ .

That is, momentum doesn't change over time... it's conserved.

$$4/ \vec{F} = -\vec{\nabla}U = \left( \frac{\partial U}{\partial x} \hat{x} + \frac{\partial U}{\partial y} \hat{y} + \frac{\partial U}{\partial z} \hat{z} \right)$$

$$F_x = (-4E) \left[ \sigma^{12} (-12) x^{-13} - \sigma^6 (-6) x^{-7} \right] \hat{x}$$

$$\vec{F}_x = -4E \left[ -\frac{12\sigma^{12}}{x^{13}} + \frac{6\sigma^6}{x^7} \right] \hat{x}$$

equilibrium is  $\vec{F}_x = 0$   $\frac{-12\sigma^{12}}{x^{13}} + \frac{6\sigma^6}{x^7} = 0$

$$\frac{12\sigma^{12}}{x^{13}} = \frac{6\sigma^6}{x^7}$$

$$2\sigma^6 = x^6$$

$$\left( 2^{1/6} \sigma = x \right)$$

5 / SHO is characterized by  $U = \frac{1}{2} kx^2$  or  $F = -kx$

$$U = -\frac{GMm}{R\sqrt{1+\frac{z^2}{R^2}}}$$

very mistake I dropped the -!

for small displacements  $z \ll R$ ,  $\left[1 + \left(\frac{z}{R}\right)^2\right]^{-1/2} \approx 1 + \left(-\frac{1}{2}\right)\left(\frac{z^2}{R^2}\right)$

$$U = -\frac{GMm}{R} \left[1 - \frac{1}{2}\left(\frac{z^2}{R^2}\right)\right]$$

$$U = \frac{GMm}{R} + \underbrace{\frac{1}{2} \frac{GMm z^2}{R^3}}$$

$$\frac{1}{2} k z^2$$

$$\text{where } k = \frac{GMm}{R^3}$$

$$\text{So } \omega = \sqrt{\frac{k}{m}} = \sqrt{\frac{GM}{R^3}}$$

$$6/ \quad F = m\ddot{x}$$

$$-kx + F_0 \cos(\omega t) = m\ddot{x}$$

$$\ddot{x} + \omega_0^2 x = \frac{F_0}{m} \cos(\omega t) \quad \text{where } \omega_0 = \sqrt{\frac{k}{m}}$$

$$\text{try } x(t) = D \cos \omega t$$

$$\ddot{x} = -\omega^2 D \cos \omega t$$

$$-\omega^2 D \cos(\omega t) + \omega_0^2 D \cos(\omega t) = \frac{F_0}{m} \cos(\omega t)$$

$$(\omega_0^2 - \omega^2) D = \frac{F_0}{m}$$

$$D = \frac{F_0/m}{\omega_0^2 - \omega^2}$$

satisfies D.E. if  
this is true

$$7/ (a) \quad \omega^2 = \omega_0^2 - \beta^2$$

$$\text{so } \beta = \sqrt{\omega_0^2 - \omega^2} = \sqrt{\left(\frac{4\pi}{1}\right)^2 - \left(\frac{2\pi}{1.005}\right)^2} = 0.63$$

$$(b) \quad A(t) = A_0 e^{-\beta t} \quad t = 10 \times T = \frac{10 \cdot 2\pi}{\omega}$$

$$\frac{A(t)}{A_0} = e^{-(0.6)(10 \cdot 1.005)}$$

$$= 0.002$$

down to 0.2% of original amplitude

8/ (a) critically damped, driven

(b) under damped

(c) under damped, driven ( $\omega_1 < \omega$ ) high frequency driving force

(d) " " ( $\omega_1 > \omega$ )

(e) free oscillator

(f) under damped

9/  $Q = \frac{\omega_R}{2\beta}$  in case of low damping  $\omega_R \hat{=} \omega_0$  (act. calc shows  $\omega_0 = 6.28$   
 $\omega_R = 6.22$ )

$$\approx \frac{2\pi}{1} = 5.2$$

Q's can be calculated for any system. It predicts behavior in the event that the system is driven: you'll be able to tell how well the system selects the resonance frequency from all the other frequencies.

10/ Yes, it does.  $D = \frac{F_0/m}{\omega_0^2 - \omega^2}$  says that the resulting

amplitude,  $D$ , depends on the driving frequency,  $\omega$ . The amplitude peaks (is undefined!) at  $\omega = \omega_0$ .

This peak in the response is <sup>the</sup> resonance phenomenon.

